

Single Span Tests **Ultimate moment in span**

test no. SSP-...	t _{cor} mm	t _{cor,obs} mm	R m	L _V m	g kN/m ²	f _{yb} N/mm ²	f _{yb,obs} N/mm ²	L m	b _v m	F _u kN	P _{vor} kN	1/μ -	F _{u,adj} kN	F _{u,adj} /F _{u,m} -	F _{u,k} kN/m	M _{c,Rk,F} kNm/m
18-0-063-1	0,527	0,527	flat	2,20	0,059	329,3	329,3	2,00	0,912	3,71	0,00	1,000	3,710	0,9521	4,112	1,057
18-0-063-2	0,527	0,527		2,20	0,059	329,3	329,3	2,00	0,912	4,07	0,00	1,000	4,070	1,0445		
18-0-063-3	0,527	0,527		2,20	0,059	329,3	329,3	2,00	0,912	3,91	0,00	1,000	3,910	1,0034		
18-30-063-1	0,527	0,527	11,5	2,20	0,059	329,3	329,3	2,00	0,912	3,97	0,00	1,000	3,970	1,0051	4,168	1,071
18-30-063-2	0,527	0,527		2,20	0,059	329,3	329,3	2,00	0,912	3,93	0,00	1,000	3,930	0,9949		
18-61-063-1	0,527	0,527	9,6	2,20	0,059	329,3	329,3	2,00	0,912	4,11	0,00	1,000	4,110	1,0123	4,284	1,100
18-61-063-2	0,527	0,527		2,20	0,059	329,3	329,3	2,00	0,912	4,01	0,00	1,000	4,010	0,9877		
18-154-063-1	0,527	0,527	4,3	2,20	0,059	329,3	329,3	2,00	0,912	4,98	0,00	1,000	4,980	1,0122	5,192	1,327
18-154-063-2	0,527	0,527		2,20	0,059	329,3	329,3	2,00	0,912	4,86	0,00	1,000	4,860	0,9878		
18-0-100-1	0,993	0,993	flat	3,20	0,093	348,7	348,7	3,00	0,912	4,10	0,00	1,000	4,100	1,0000	4,326	1,727
18-64-100-1	0,993	0,993	17,2	3,20	0,093	348,7	348,7	3,00	0,912	4,20	0,00	1,000	4,200	1,0182	4,353	1,736
18-64-100-2	0,993	0,993		3,20	0,093	348,7	348,7	3,00	0,912	4,10	0,00	1,000	4,100	0,9939		
18-64-100-3	0,993	0,993		3,20	0,093	348,7	348,7	3,00	0,912	4,10	0,00	1,000	4,100	0,9939		
18-64-100-4	0,993	0,993		3,20	0,093	348,7	348,7	3,00	0,912	4,10	0,00	1,000	4,100	0,9939		
18-129-100-1	0,993	0,993	10,6	3,20	0,093	348,7	348,7	3,00	0,912	4,00	0,00	1,000	4,000	1,0084	4,186	1,674
18-129-100-2	0,993	0,993		3,20	0,093	348,7	348,7	3,00	0,912	4,00	0,00	1,000	4,000	1,0084		
18-129-100-3	0,993	0,993		3,20	0,093	348,7	348,7	3,00	0,912	3,90	0,00	1,000	3,900	0,9832		
18-334-100-1	0,993	0,993	3,8	3,20	0,093	348,7	348,7	3,00	0,912	3,80	0,00	1,000	3,800	0,9661	4,151	1,661
18-334-100-2	0,993	0,993		3,20	0,093	348,7	348,7	3,00	0,912	4,00	0,00	1,000	4,000	1,0169		
18-334-100-3	0,993	0,993		3,20	0,093	348,7	348,7	3,00	0,912	4,00	0,00	1,000	4,000	1,0169		
39-0-063-1	0,580	0,580	flat	3,20	0,060	408,3	408,3	3,00	1,000	2,09	0,00	1,000	2,090	1,0503	1,915	0,785
39-0-063-2	0,580	0,580		3,20	0,060	408,3	408,3	3,00	1,000	2,03	0,00	1,000	2,030	1,0201		
39-0-063-2	0,580	0,580		3,20	0,060	408,3	408,3	3,00	1,000	1,85	0,00	1,000	1,850	0,9296		
39-64-063-1	0,580	0,580	32,9	3,20	0,060	408,3	408,3	3,00	1,000	1,92	0,00	1,000	1,920	0,9897	1,867	0,767
39-64-063-2	0,580	0,580		3,20	0,060	408,3	408,3	3,00	1,000	1,96	0,00	1,000	1,960	1,0103		
39-129-063-1	0,580	0,580	9,7	3,20	0,060	408,3	408,3	3,00	1,000	1,84	0,00	1,000	1,840	0,9973	1,776	0,733
39-129-063-2	0,580	0,580		3,20	0,060	408,3	408,3	3,00	1,000	1,85	0,00	1,000	1,850	1,0027		
39-217-063-1	0,580	0,580	5,6	3,20	0,060	408,3	408,3	3,00	1,000	1,61	0,00	1,000	1,610	1,0021	1,546	0,647
39-217-063-2	0,580	0,580		3,20	0,060	408,3	408,3	3,00	1,000	1,56	0,00	1,000	1,560	0,9710		
39-217-063-3	0,580	0,580		3,20	0,060	408,3	408,3	3,00	1,000	1,65	0,00	1,000	1,650	1,0270		
39-0-100-1	0,957	0,957	flat	4,20	0,095	381,7	381,7	4,00	1,000	2,80	0,00	1,000	2,800	0,9982	2,699	1,539
39-0-100-2	0,957	0,957		4,20	0,095	381,7	381,7	4,00	1,000	2,81	0,00	1,000	2,810	1,0018		
39-111-100-1	0,957	0,957	25,8	4,20	0,095	381,7	381,7	4,00	1,000	2,78	0,00	1,000	2,780	1,0109	2,646	1,513
39-111-100-2	0,957	0,957		4,20	0,095	381,7	381,7	4,00	1,000	2,72	0,00	1,000	2,720	0,9891		
39-223-100-1	0,957	0,957	10,6	4,20	0,095	381,7	381,7	4,00	1,000	2,81	0,00	1,000	2,810	0,9982	2,709	1,544
39-223-100-2	0,957	0,957		4,20	0,095	381,7	381,7	4,00	1,000	2,82	0,00	1,000	2,820	1,0018		
39-380-100-1	0,957	0,957	6,4	4,20	0,095	381,7	381,7	4,00	1,000	2,82	0,00	1,000	2,820	0,9947	2,728	1,554
39-380-100-2	0,957	0,957		4,20	0,095	381,7	381,7	4,00	1,000	2,85	0,00	1,000	2,850	1,0053		

number	38	s	38,000
EC	k =	1,73	(1-k-s) 0,0218
			0,9624

Single Span Tests with horizontal supports

Characteristic failure load

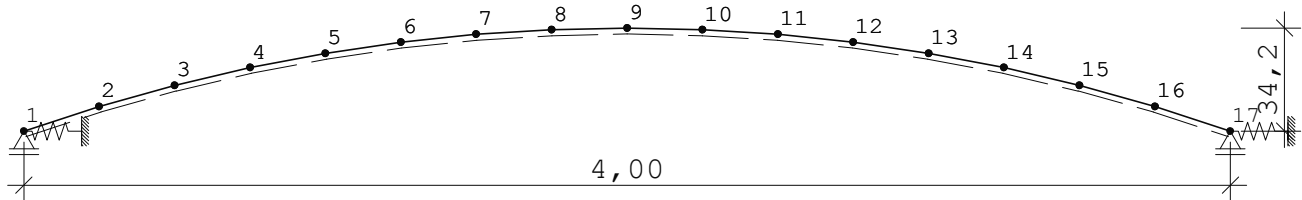
test no. SSP-H-39-...	t_{cor} mm	$t_{cor,obs}$ mm	R m	L_V m	g kN/m ²	f_{yb} N/mm ²	$f_{yb,obs}$ N/mm ²	L m	b_V m	F_u kN	P_{vor} kN	$1/\mu$ -	$F_{u,adj}$ kN	$F_{u,adj}/F_{u,m}$ -	$F_{u,k}$ kN/m	
217-063-1	0,580	0,580	5,56	3,20	0,060	408,3	408,3	3,00	0,667	9,12	0,00	1,000	9,120	1,0094	11,027	
217-063-2	0,580	0,580		3,20	0,060	408,3	408,3	3,00	0,667	8,95	0,00	1,000	8,950	0,9906		
380-063-1	0,580	0,580	6,02	4,20	0,060	408,3	408,3	4,00	0,667	9,49	0,00	1,000	9,490	0,8911	12,767	
380-063-2	0,580	0,580		4,20	0,060	408,3	408,3	4,00	0,667	11,43	0,00	1,000	11,430	1,0732		
380-063-3	0,580	0,580		4,20	0,060	408,3	408,3	4,00	0,667	11,03	0,00	1,000	11,030	1,0357		
576-063-1	0,580	0,580	7,04	5,20	0,060	408,3	408,3	5,00	0,667	5,67	0,00	1,000	5,670	0,9626	6,615	
576-063-2	0,580	0,580		5,20	0,060	408,3	408,3	5,00	0,667	5,17	0,00	1,000	5,170	0,8778		
576-063-3	0,580	0,580		5,20	0,060	408,3	408,3	5,00	0,667	6,83	0,00	1,000	6,830	1,1596		
												number	8	8,000		
												EC	k =	2,00	s	0,0930
															(1-k·s)	0,8141

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PLANE FRAME ANALYSIS ESK1 06/2003 WinVista sheet 1

PROJECT: 003 GRISPE - Curved profiles SUB: AR-4g-te
Name: Arch Span 4 m C 62 (test)

System scale 1 : 25



MATERIAL : Sonstiges E-modulus E = 21000 kN/cm² GammaM = 1.00
unit weight : 7.85 kg/dm³

SECTION PROPERTIES

Cross-sect. No.	Profile Mat	Name	I (cm ⁴)	A (cm ²)	A _q (cm ²)	h (cm)	S top (cm ³)	S bot (cm ³)
1	1	Arcelor 3	9.77	6.58	0.000	0.00	0.000	0.000
2	1	Arcelor 3	5.21	1.89	0.000	0.00	0.000	0.000

Cross section 1 : Arcelor 39-0,63-Ag

Cross section 2 : Arcelor 39-0,63-Aef

SYSTEM	Projections		Cross-section		Nodes	
Member	Lx (m)	Lz (m)	Q1	Q2	End 1	End 2
1	0.250	0.082	1	1	1.0	2.0
2	0.250	0.070	1	1	2.0	3.0
3	0.250	0.059	1	1	3.0	4.0
4	0.250	0.047	1	1	4.0	5.0
5	0.250	0.037	1	1	5.0	6.0
6	0.250	0.026	1	1	6.0	7.0
7	0.250	0.015	1	1	7.0	8.0
8	0.250	0.006	1	1	8.0	9.0
9	0.250	-0.006	1	1	9.0	10.0
10	0.250	-0.015	1	1	10.0	11.0
11	0.250	-0.026	1	1	11.0	12.0
12	0.250	-0.037	1	1	12.0	13.0
13	0.250	-0.047	1	1	13.0	14.0
14	0.250	-0.059	1	1	14.0	15.0
15	0.250	-0.070	1	1	15.0	16.0
16	0.250	-0.082	1	1	16.0	17.0

SUPPORTS : -1 = rigid , 0 = free , > 0 = elastic (kN/cm , kNcm)

Node	horizontal	vertical	rotating
1	62.00	-1	0
17	62.00	-1	0

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PLANE FRAME ANALYSIS ESK1 06/2003 WinVista sheet 2

PROJECT: 003 GRISPE - Curved profiles SUB: AR-4g-te
Name: Arch Span 4 m C 62 (test)

Nodes		C o o r d i n a t e s		Differences	
No.	x (m)	z (m)	d x (m)	d z	
1	-2.000	0.000			
2	-1.750	0.082			
3	-1.500	0.152			
4	-1.250	0.211			
5	-1.000	0.258			
6	-0.750	0.295			
7	-0.500	0.321			
8	-0.250	0.336			
9	0.000	0.342			
10	0.250	0.336			
11	0.500	0.321			
12	0.750	0.295			
13	1.000	0.258			
14	1.250	0.211			
15	1.500	0.152			
16	1.750	0.082			
17	2.000	0.000			

Weight of construction G = 21 kg

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PLANE FRAME ANALYSIS ESK1 06/2003 WinVista sheet 3

PROJECT: 003 GRISPE - Curved profiles SUB: AR-4g-te
 Name: Arch Span 4 m C 62 (test)

L O A D I N G No. 4 Load case : char failure load

Nodal loads

Node	Force H	Force V	Moment M	(kN)	(kNm)
3	0.000	3.193	0.000		
7	0.000	3.193	0.000		
11	0.000	3.193	0.000		
15	0.000	3.193	0.000		

Sum of all external loads (kN)

Total	Fx	Fz
	0.000	12.772

Maximum displacement in member 9 at $x = 0.00 * L$ Max_f = 1.44 cm

SUPPORT REACTIONS Th. 1.Ord. Load case 4 : char failure load

Node	Force H	Force V	Moment M	(kN)	(kNm)
1	-18.636	6.386			
17	18.636	6.386			
Sum :	0.000	12.772			

INTERNAL FORCES Th. 1.Ord. Load case 4 : char failure load

member No.	Q No.	node No.	Q (kN)	N (kN)	M (kNm)
1	1	1	0.26	-19.70	0.00
		.50	0.26	-19.70	0.03
		2	0.26	-19.70	0.07
2	1	2	1.12	-19.67	0.07
		.50	1.12	-19.67	0.21
		3	1.12	-19.67	0.36
3	1	3	-1.17	-18.87	0.36
		.50	-1.17	-18.87	0.21
		4	-1.17	-18.87	0.06
4	1	4	-0.31	-18.90	0.06
		.50	-0.31	-18.90	0.02
		5	-0.31	-18.90	-0.02
5	1	5	0.43	-18.90	-0.02
		.50	0.43	-18.90	0.04
		6	0.43	-18.90	0.09
6	1	6	1.25	-18.87	0.09
		.50	1.25	-18.87	0.25

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PLANE FRAME ANALYSIS ESK1 06/2003 WinVista sheet 4

PROJECT: 003 GRISPE - Curved profiles SUB: AR-4g-te
 Name: Arch Span 4 m C 62 (test)

INTERNAL FORCES Th. 1.Ord. Load case 4 : char failure load

member No.	Q No.	node No.	Q (kN)	N (kN)	M (kNm)
	1	7	1.25	-18.87	0.40
7	1	7	-1.12	-18.60	0.40
	.50		-1.12	-18.60	0.26
	1	8	-1.12	-18.60	0.12
8	1	8	-0.45	-18.63	0.12
	.50		-0.45	-18.63	0.07
	1	9	-0.45	-18.63	0.01
9	1	9	0.45	-18.63	0.01
	.50		0.45	-18.63	0.07
	1	10	0.45	-18.63	0.12
10	1	10	1.12	-18.60	0.12
	.50		1.12	-18.60	0.26
	1	11	1.12	-18.60	0.40
11	1	11	-1.25	-18.87	0.40
	.50		-1.25	-18.87	0.25
	1	12	-1.25	-18.87	0.09
12	1	12	-0.43	-18.90	0.09
	.50		-0.43	-18.90	0.04
	1	13	-0.43	-18.90	-0.02
13	1	13	0.31	-18.90	-0.02
	.50		0.31	-18.90	0.02
	1	14	0.31	-18.90	0.06
14	1	14	1.17	-18.87	0.06
	.50		1.17	-18.87	0.21
	1	15	1.17	-18.87	0.36
15	1	15	-1.12	-19.67	0.36
	.50		-1.12	-19.67	0.21
	1	16	-1.12	-19.67	0.07
16	1	16	-0.26	-19.70	0.07
	.50		-0.26	-19.70	0.03
	1	17	-0.26	-19.70	0.00

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PLANE FRAME ANALYSIS ESK1 06/2003 WinVista sheet 5

PROJECT: 003 GRISPE - Curved profiles SUB: AR-4g-te
 Name: Arch Span 4 m C 62 (test)

DISPLACEMENTS Th. 1.Ord. Load case 4 : char failure load

Node No.	Displacement u (cm)	Displacement v (cm)	Rotation r
1	-0.30057	0.00000	0.01356
2	-0.19415	0.33648	0.01312
3	-0.11321	0.63928	0.01041
4	-0.06482	0.85959	0.00778
5	-0.03264	1.04961	0.00753
6	-0.00860	1.23562	0.00709
7	0.00331	1.38333	0.00406
8	0.00319	1.43762	0.00084
9	0.00000	1.44530	0.00000
10	-0.00319	1.43762	-0.00084
11	-0.00331	1.38333	-0.00406
12	0.00860	1.23562	-0.00709
13	0.03264	1.04961	-0.00753
14	0.06482	0.85959	-0.00778
15	0.11321	0.63928	-0.01041
16	0.19415	0.33648	-0.01312
17	0.30057	0.00000	-0.01356

DISPLACEMENT OF SPANS (cm) Th. 1.Ord. Load case 4 : char failure load

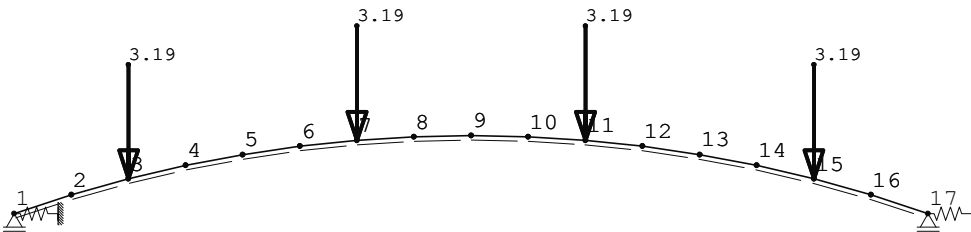
Member No.	End 1									End 2
	0	1/8	2/8	3/8	x/L = 4/8	5/8	6/8	7/8	1	
1	-0.09	-0.05	0.00	0.04	0.08	0.13	0.17	0.22	0.26	0.26
2	0.27	0.31	0.36	0.40	0.44	0.48	0.51	0.55	0.59	0.59
3	0.60	0.63	0.66	0.69	0.72	0.74	0.77	0.80	0.82	0.82
4	0.83	0.86	0.88	0.91	0.93	0.95	0.98	1.00	1.03	1.03
5	1.03	1.06	1.08	1.10	1.13	1.15	1.18	1.20	1.22	1.22
6	1.23	1.25	1.27	1.29	1.31	1.33	1.35	1.36	1.38	1.38
7	1.38	1.39	1.40	1.41	1.42	1.42	1.43	1.43	1.44	1.44
8	1.44	1.44	1.44	1.44	1.44	1.44	1.44	1.44	1.44	1.44
9	1.44	1.44	1.44	1.44	1.44	1.44	1.44	1.44	1.44	1.44
10	1.44	1.43	1.43	1.42	1.42	1.41	1.40	1.39	1.38	1.38
11	1.38	1.36	1.35	1.33	1.31	1.29	1.27	1.25	1.23	1.23
12	1.22	1.20	1.18	1.15	1.13	1.10	1.08	1.06	1.03	1.03
13	1.03	1.00	0.98	0.95	0.93	0.91	0.88	0.86	0.83	0.83
14	0.82	0.80	0.77	0.74	0.72	0.69	0.66	0.63	0.60	0.60
15	0.59	0.55	0.51	0.48	0.44	0.40	0.36	0.31	0.27	0.27
16	0.26	0.22	0.17	0.13	0.08	0.04	0.00	-0.05	-0.09	-0.09

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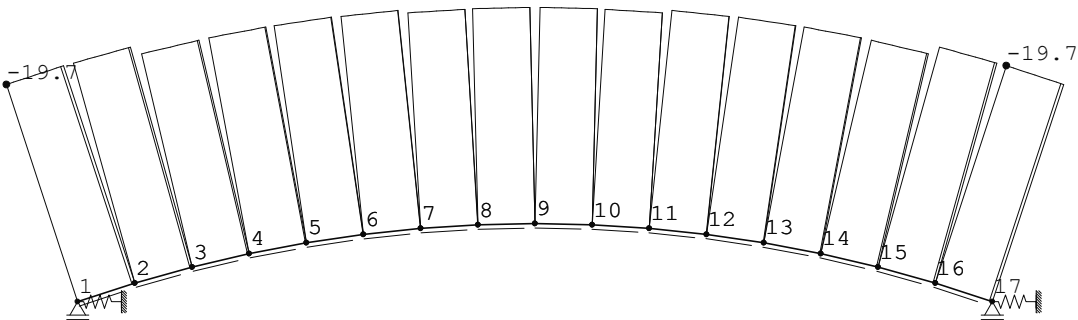
PLANE FRAME ANALYSIS ESK1 06/2003 WinVista sheet 6

PROJECT: 003 GRISPE - Curved profiles SUB: AR-4g-te
 Name: Arch Span 4 m C 62 (test)

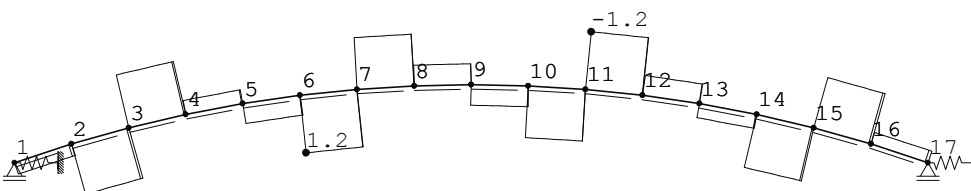
Loads load case no. 4 M 1 : 33



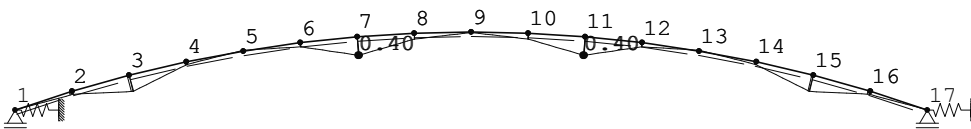
Normal force (kN) load case no. 4 Th.2.Ord. M 1 : 33



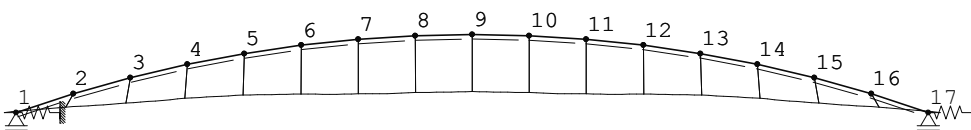
Shear force (kN) load case no. 4 Th.2.Ord. M 1 : 33



Moments (kNm) load case no. 4 Th.2.Ord. M 1 : 33



Displacement (cm) load case no. 4 Th.2.Ord. M 1 : 33



Failure load compared with M-N-interaction formula according to DIN 18807

Test setup/ span	Cross section	spring stiffness at support (kN/m/cm)	M- / N-values (kNm/m, kN/m)		relative m M/M ₀	DIN 18807 with limit $\alpha < 1$		DIN 18807 without limit α		system parameters	
			at load point near to summit max M	at support max N		relative n N/N _{ED} * [1+0,5 α ...]	m + n	relative n N/N _{ED} * [1+0,5 α ...]	m + n		
1 / 3,00 m	gross	fixed	0,17	20,62	0,156	slenderness $\alpha =$	1,297	slenderness $\alpha =$	1,297	arch height (mm)	206,3
		68,0	0,49	18,98	0,448	$\sigma_{\text{ed}} / f_{\text{yk}} =$	0,583	$\sigma_{\text{ed}} / f_{\text{yk}} =$	0,583	arch length (mm)	3,038
		20,0	1,08	15,94	0,988	ult N _{ED} = (kN/m)	44,95	ult N _{ED} = (kN/m)	44,95	f/l =	0,069
	effective	10,0	1,65	13,01	1,510	decisive N _{ED} =	44,95	decisive N _{ED} =	44,95	coefficient β	1,01
		fixed	0,19	20,51	0,174					buckling length s _k	1,534
		88,0	0,33	19,80	0,302					max N _{ED} = (kN/m)	68,82
2 / 4,00 m	gross	20,0	0,73	17,74	0,668	slenderness $\alpha =$	1,758	slenderness $\alpha =$	1,758	arch height (mm)	341,7
		10,0	1,14	15,64	1,043	$\sigma_{\text{ed}} / f_{\text{yk}} =$	0,390	$\sigma_{\text{ed}} / f_{\text{yk}} =$	0,390	arch length (mm)	4,077
		fixed	0,25	19,35	0,229	ult N _{ED} = (kN/m)	30,06	ult N _{ED} = (kN/m)	30,06	f/l =	0,085
	effective	62,0	0,40	18,87	0,366	decisive N _{ED} =	30,06	decisive N _{ED} =	30,06	coefficient β	1,02
		20,0	0,71	17,92	0,650					buckling length s _k	2,079
		10,0	1,11	16,69	1,016					max N _{ED} = (kN/m)	37,47
3 / 5,00 m	gross	fixed	0,26	19,31	0,238	slenderness $\alpha =$	2,204	slenderness $\alpha =$	2,204	arch height (mm)	459,2
		79,0	0,33	19,11	0,302	$\sigma_{\text{ed}} / f_{\text{yk}} =$	0,247	$\sigma_{\text{ed}} / f_{\text{yk}} =$	0,247	arch length (mm)	5,112
		20,0	0,51	18,53	0,467	ult N _{ED} = (kN/m)	19,06	ult N _{ED} = (kN/m)	19,06	f/l =	0,092
	effective	10,0	0,75	17,80	0,686	decisive N _{ED} =	19,06	decisive N _{ED} =	19,06	coefficient β	1,02
		fixed	0,16	9,36	0,146					buckling length s _k	2,607
		29,0	0,26	9,14	0,238					max N _{ED} = (kN/m)	23,83
3 / 5,00 m	gross	20,0	0,30	9,04	0,274	slenderness $\alpha =$	2,204	slenderness $\alpha =$	2,204	arch height (mm)	459,2
		10,0	0,43	8,74	0,393	$\sigma_{\text{ed}} / f_{\text{yk}} =$	0,247	$\sigma_{\text{ed}} / f_{\text{yk}} =$	0,247	arch length (mm)	5,112
		fixed	0,16	9,35	0,146	ult N _{ED} = (kN/m)	19,06	ult N _{ED} = (kN/m)	19,06	f/l =	0,092
	effective	33,0	0,21	9,09	0,192	decisive N _{ED} =	19,06	decisive N _{ED} =	19,06	coefficient β	1,02
		20,0	0,24	9,18	0,220					buckling length s _k	2,607
		10,0	0,31	9,01	0,284					max N _{ED} = (kN/m)	23,83

green coloured lines: spring stiffness at support adapted to the midspan-deflection in test.

red values interaction formula is unsafe (calculated superposition in failure state < 1)

blue values interaction formula is safe (calculated superposition in failure state > 1)

Failure load compared with M-N-interaction formula according to EN 1993-1-3, buckling curve b and c

Test setup/ span	Cross section	spring stiffness at support (kN/m/cm)	M- / N-values (kNm/m, kN/m)		relative m M/M _u	EN 1993 buckling curve b		EN 1993 buckling curve c		system parameters		
			at load point near to summit	at support max N		relative n N/N _{Ed}	m ^{0.8} + n ^{0.8}	relative n N/N _{Ed}	m ^{0.8} + n ^{0.8}		α =	α =
1 / 3,00 m	gross	fixed	0.17	20,62	21,19	0,156	0,624	1,297	0,685	0,96	slenderness λ = 1,297	arch height (mm) 206,3
		68,0	0,49	18,98	19,60	0,448	0,574	1,527	0,631	1,22	φ = 1,610	arch length (mm) 3,038
		20,0	1,08	15,94	16,65	0,988	0,482	0,428	0,530	1,59	X = 0,390	f/l = 0,069
	effective	10,0	1,65	13,01	13,80	1,510	0,394	33,05	0,432	1,90	ult N _{Ed} = (kN/m)	coefficient β 1,01
		fixed	0,19	20,51	21,08	0,174	0,621	33,05	0,681	0,98	decisive N _{Ed} = 30,10	buckling length s _k 1,534
		88,0	0,33	19,80	20,40	0,302	0,599		0,658	1,10	max N _{Ed} = (kN/m) 68,82	
2 / 4,00 m	gross	fixed	0.25	19,35	20,16	0,229	0,955	1,758	1,028	1,33	slenderness λ = 1,758	arch height (mm) 341,7
		62,0	0,40	18,87	19,70	0,366	0,931	2,309	1,002	1,45	φ = 2,426	arch length (mm) 4,077
		20,0	0,71	17,92	18,80	0,650	0,884	0,263	0,952	1,67	X = 0,244	f/l = 0,085
	effective	10,0	1,11	16,69	17,62	1,016	0,824	20,26	0,887	1,92	ult N _{Ed} = (kN/m)	coefficient β 1,02
		fixed	0,26	19,31	20,13	0,238	0,953	20,26	1,026	1,34	decisive N _{Ed} = 18,82	buckling length s _k 2,079
		79,0	0,33	19,11	19,93	0,302	0,943		1,015	1,40	max N _{Ed} = (kN/m) 37,47	
3 / 5,00 m	gross	fixed	0.16	9,36	9,81	0,146	0,689	2,204	0,732	0,99	slenderness λ = 2,204	arch height (mm) 459,2
		29,0	0,26	9,14	9,60	0,238	0,673	3,269	0,715	1,08	φ = 3,419	arch length (mm) 5,112
		20,0	0,30	9,04	9,50	0,274	0,666	0,176	0,707	1,11	X = 0,166	f/l = 0,092
	effective	10,0	0,43	8,74	9,22	0,393	0,644	13,58	0,683	1,21	ult N _{Ed} = (kN/m)	coefficient β 1,02
		fixed	0,16	9,35	9,80	0,146	0,689	13,58	0,731	0,99	decisive N _{Ed} = 12,79	buckling length s _k 2,607
		33,0	0,21	9,09	9,70	0,192	0,670		0,711	1,03	max N _{Ed} = (kN/m) 23,83	
effective	20,0	0,24	9,18	9,63	0,220	0,676		0,718	1,06			
	10,0	0,31	9,01	9,48	0,284	0,664		0,705	1,12			

green coloured lines: spring stiffness at support adapted to the midspan-deflection in test.

red values interaction formula is unsafe (calculated superposition in failure state < 1)

blue values interaction formula is safe (calculated superposition in failure state > 1)